

# EFFECT OF MATERIALS HETEROGENEITIES ON MICROSTRUCTURE AND MECHANICAL PROPERTIES AT IRRADIATED STATE

## Authors

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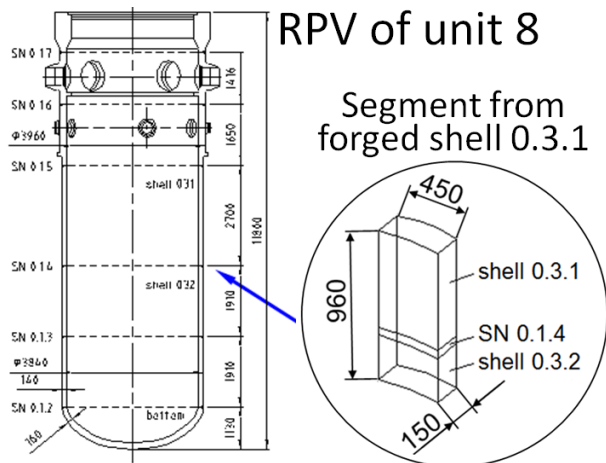
Contributors of Task 3.3 (CIEMAT, CNRS,  
Framatome, NRI, VTT)



- ❑ Material FZD-4 (HZDR + CIEMAT)
  - basic information, initial microstructure and properties
  - irradiation-induced microstructure and property changes
- ❑ Material EDF-4 (CNRS)
  - basic information, initial microstructure and properties
  - irradiation-induced microstructure
- ❑ Materials NRI-1/2 (NRI)
  - basic information, initial microstructure and properties
  - irradiation hardening
- ❑ Materials ANP-3/4 + VTT-1/WM1 (VTT + Framatome)
  - basic information
  - MC and cleavage initiation sites for irradiated condition

# FZD-4: basic information (1)

- ❑ NPP Greifswald, RPV of Unit 8, VVER440-type base metal 15Kh2MFAA
- ❑ RPV of Unit 8 completed in 1989 (Škoda production), non-commissioned
- ❑ Identical in construction with operating NPPs at Dukovany, Bohunice, Mochovce, Paks



Composition of 15Kh2MFAA forged ring 0.3.1 (wt. %)

	C	Si	Mn	Cr	Ni	Mo	Cu	P	V
HZDR analysis	0.15	0.30	0.45	2.86	0.10	0.79	0.05	0.008	0.31
Documentation	0.16	0.25	0.49	2.82	0.09	0.72	0.05	0.01	0.29

## FZD-4: basic information (2)

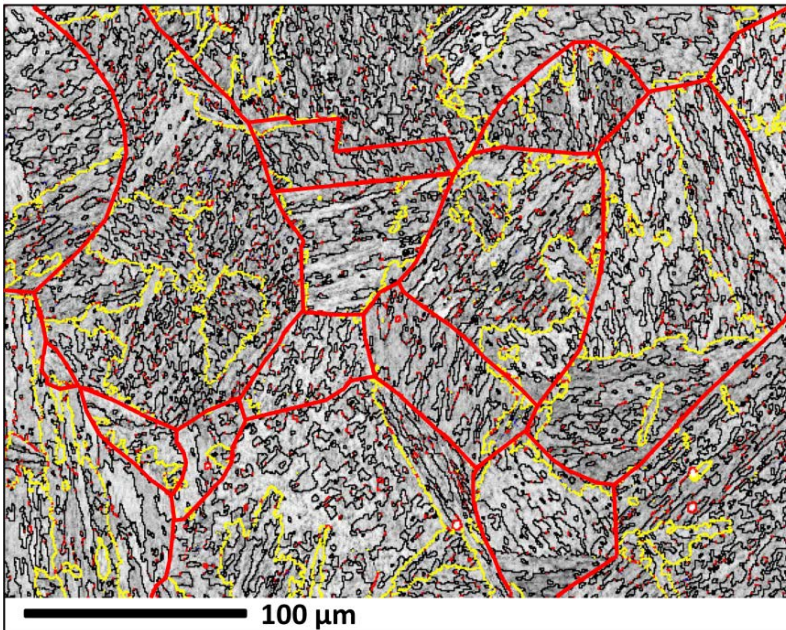
- ❑ Irradiated at HFR Petten (LYRA 9) and KFKI Budapest (BAGIRA - Budapest Advanced Gas-cooled Irradiation Rig with Aluminium structure)
- ❑ Reported irradiation conditions:

Irradiation experiment	Neutron fluence ( $10^{19} \text{ cm}^{-2}$ ) ( $E > 1 \text{ MeV}$ )	Neutron flux ( $10^{12} \text{ cm}^{-2}\text{s}^{-1}$ ) ( $E > 1 \text{ MeV}$ )	Irradiation temperature ( $^{\circ}\text{C}$ )	Irradiation time (full power days)
Lyra 9	2.6	1.1	270	272
Bagira C	11.7	34.8	290	49
Bagira A	18.2	54.1	290	49
Bagira B	20.8	61.9	290	49

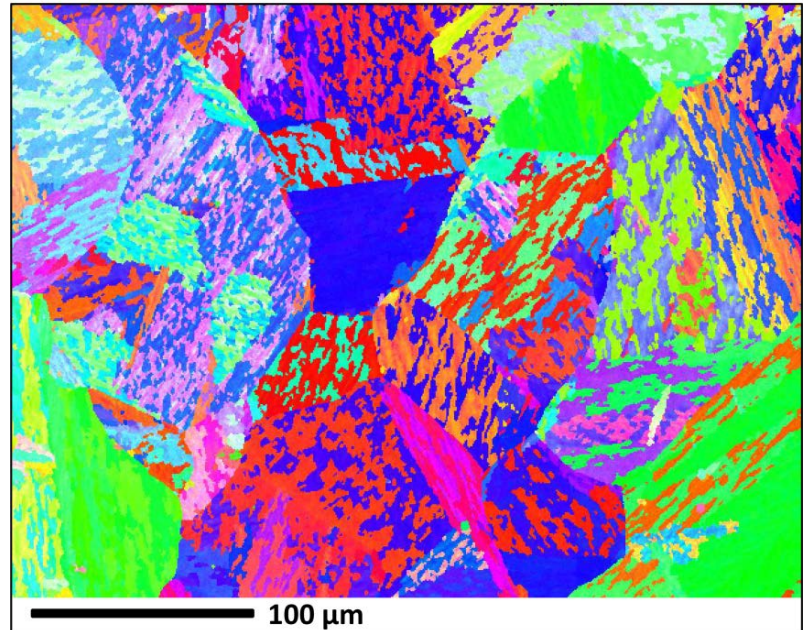
# FZD-4: initial microstructure (1)

- ❑ EBSD reveals a bainitic microstructure with former austenite grains ( $\sim 110 \mu\text{m}$ ), packets ( $\sim 30 \mu\text{m}$ ) and blocks ( $9 \mu\text{m}$ )
- ❑ EBSD provides details about the variant selection during the bainitic transformation

Austenite grain boundaries and block/packet boundaries:



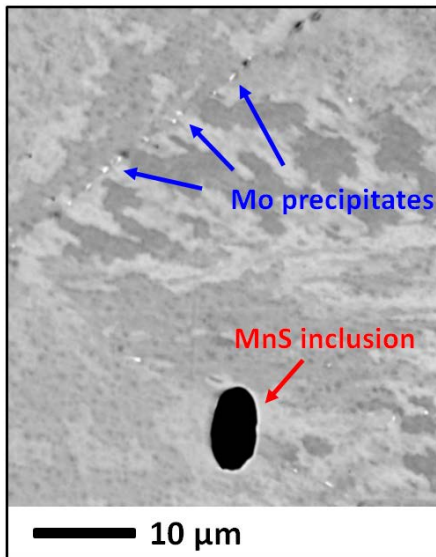
IPF-X plot:





# FZD-4: initial microstructure (2)

- ❑ Hierarchically organized precipitates and inclusions that differ in their size and density over several orders of magnitude
- ❑ Location is related to bainitic grain structure

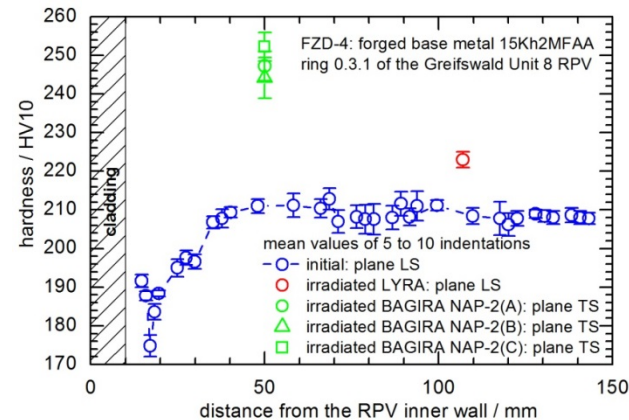


Type	Mean size (µm)	Number density (cm <sup>-3</sup> )	Preferred location
Very small V-rich (TEM)	0.02	2.7E+14	Matrix
V-rich (TEM)	0.14	3.8E+13	Packet/block boundaries
Cr-rich (TEM)	0.2	1.0E+13	Packet/block boundaries
Mo-rich (SEM)	0.4	1E+10	γ-grain boundaries
Coarse MnS (SEM)	8	3E+06	-

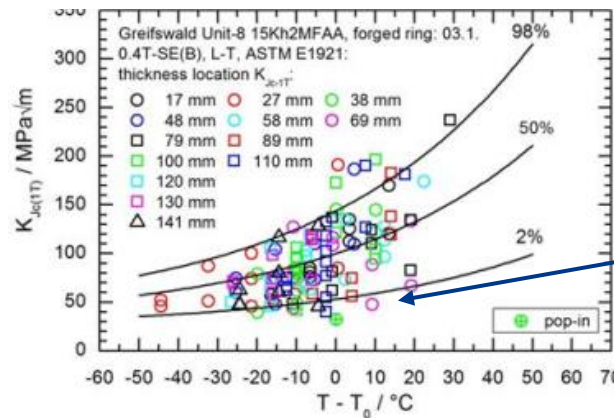
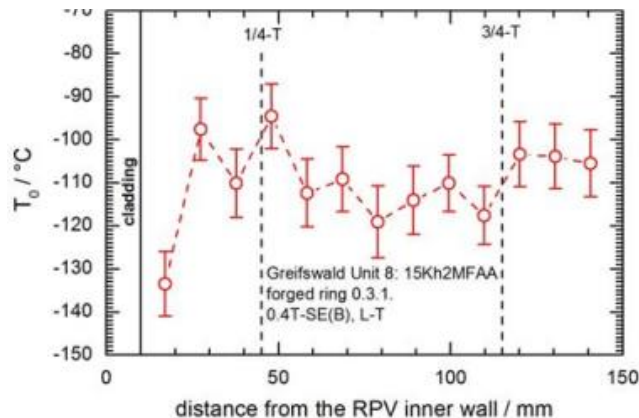
- ❑ CIEMAT: Spatial variations of dislocation density, mean value  $\rho = 2.6E+14 \text{ m}^{-2}$

# FZD-4: initial properties (1)

- Through-thickness distribution of hardness



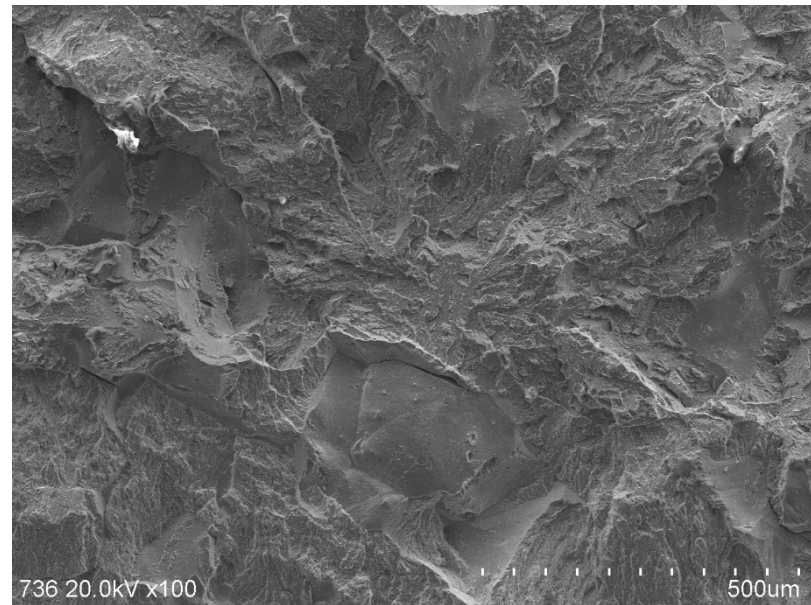
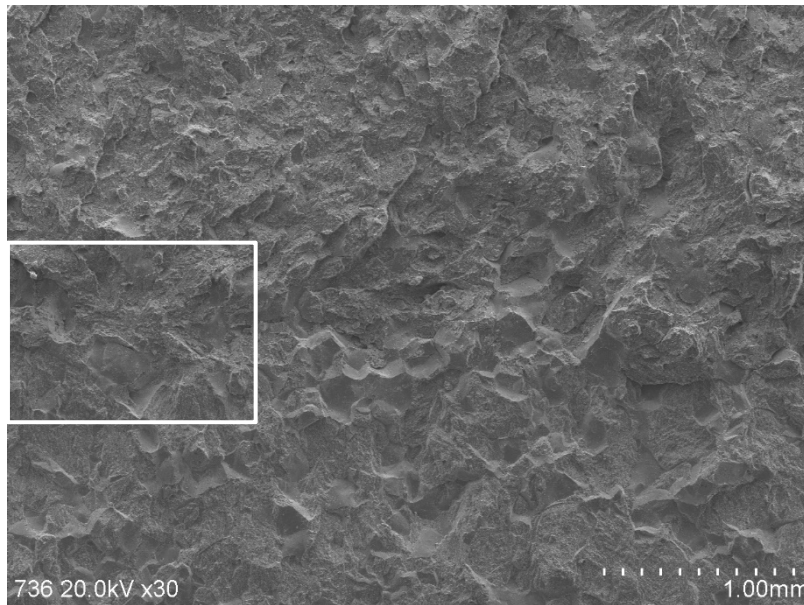
- Through-thickness distribution of MC- $T_0$  (left) and temperature-adjusted MC for all data (right)



9 out of 98 data points are below the 2% tolerance bound!

# FZD-4: initial properties (2)

- ❑ Possible reason for large scatter: Local appearance of intergranular fracture (23% fatigue crack, 11% cleavage crack)



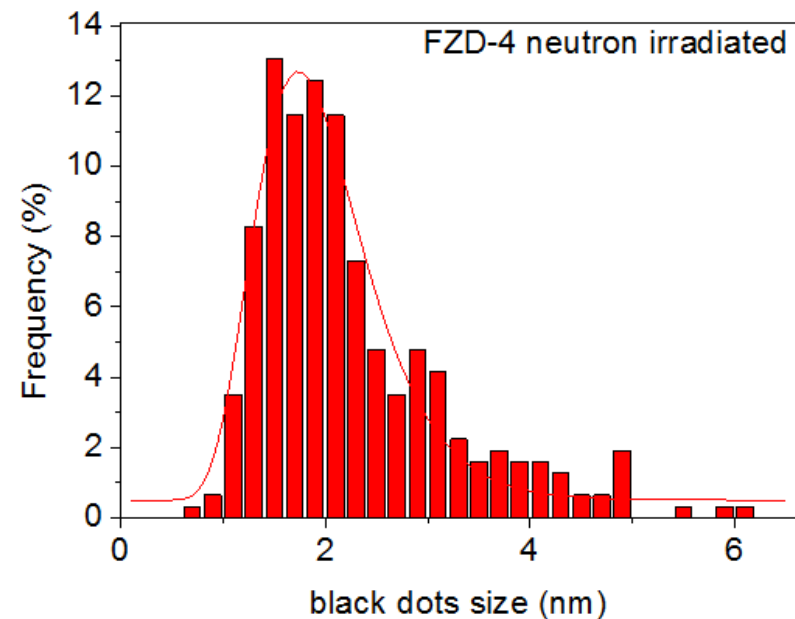
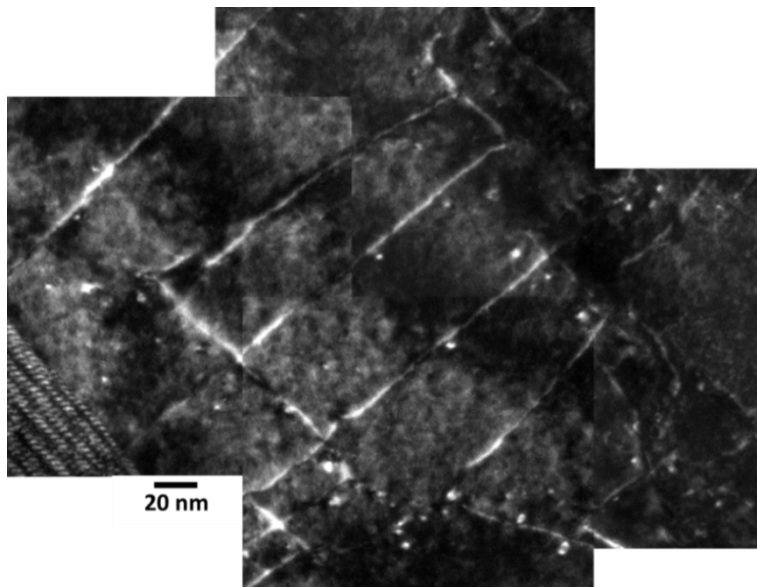
- ❑ Consistent with AES evidence (CIEMAT): P enrichment at GBs found at intergranular fracture planes
- ❑ Consequence: MC approach not applicable → multimodal MC



# FZD-4: irradiated microstructure (1)

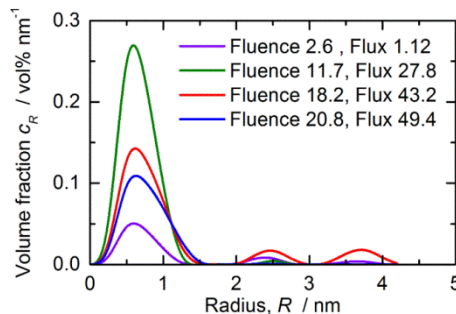
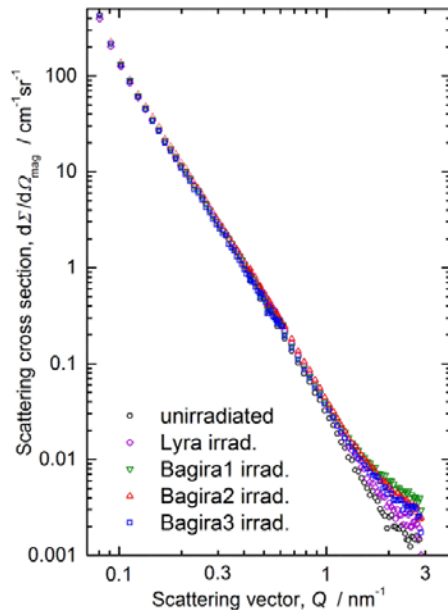
## □ TEM (CIEMAT)

- BAGIRA (B) irradiation:  $20.8\text{E}+19 \text{ cm}^{-2}$  ( $E > 1 \text{ MeV}$ ),  $290^\circ\text{C}$
- Dislocation loops observed, mostly closely to line dislocations
- Mean size 1.9 nm, Number density  $2\text{E}+15 \text{ cm}^{-3}$  ( $g=110$ )
- No/very few defects detectable for RPV steels at lower fluences



# FZD-4: irradiated microstructure (2)

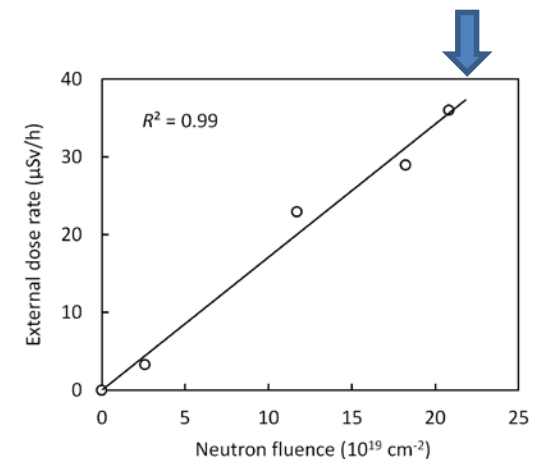
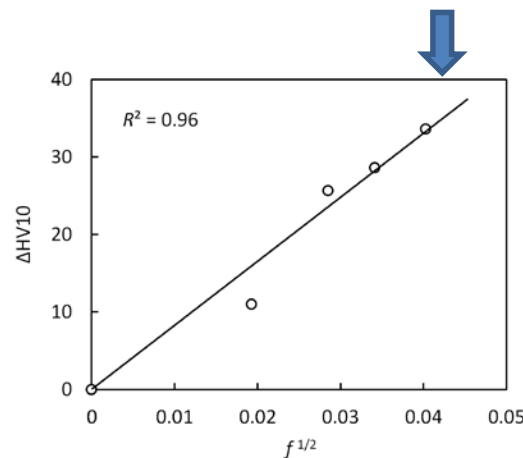
## □ SANS (HZDR, beamline V4 at HZB Berlin)



Irradiation experiment	Neutron fluence (10 <sup>19</sup> cm <sup>-2</sup> )	Volume fraction (vol%)	Mean radius (nm)	A-ratio (-)	Vickers hardness, HV10 (-)	ΔHV10 (-)
unirradiated	0	0	-	-	218.5 ± 1.9	0
Lyra	2.6	0.037 ± 0.003	0.83 ± 0.06	1.5 ± 0.2	229.5 ± 3.9	11 ± 5
Bagira (C)	11.7	0.162 ± 0.005	0.76 ± 0.07	2.0 ± 0.2	252.2 ± 3.7	34 ± 5
Bagira (A)	18.2	0.116 ± 0.005	0.78 ± 0.05	3.0 ± 0.5	247.2 ± 3.8	29 ± 5
Bagira (B)	20.8	0.081 ± 0.004	0.78 ± 0.04	2.0 ± 0.2	244.2 ± 5.3	26 ± 6

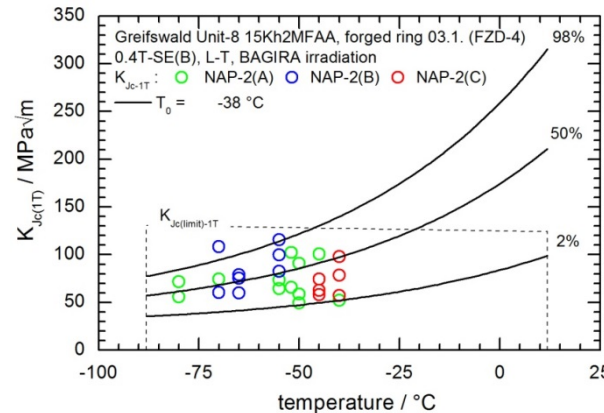
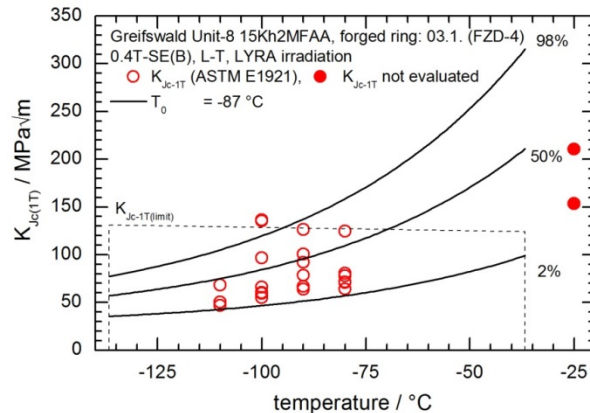
□ BAGIRA irradiations: Decreasing volume fraction at increasing fluence → Contradiction

□ Reason: Exp. error? No! // Mix-up of samples? No!



# FZD-4: irradiated properties

## □ MC for LYRA (left) and BAGIRA (right) irradiations



Data scatter for irr. conditions are smaller than for the initial condition

Irradiation experiment	Neutron fluence ( $10^{19} \text{ cm}^{-2}$ ) ( $E > 1 \text{ MeV}$ )	Volume fraction (vol%)	$\Delta \text{HV}_{10}$ (-)	$\Delta T_0$ (K)
Lyra 9	2.6	0.037	11	24
Bagira C	11.7	0.162	34	97
Bagira A	18.2	0.116	29	80
Bagira B	20.8	0.081	26	61

MC  $T_0$  shift also decreases with increasing fluence

→ any material inhomogeneity can be excluded as reason, because samples were taken from random positions

- ❑ In the initial condition, large scatter of fracture toughness (MC not applicable) and spatial variations of the fracture mode (inter- or trans-granular) were observed.
- ❑ In the as-irradiated condition, the scatter is reduced, intergranular fracture occurs as well.
- ❑ The reduction of scatter can be rationalized by the fact that smaller precipitates (available at higher number) may trigger crack initiation for the irradiated condition.
- ❑ Reductions of volume fraction,  $\Delta HV_{10}$  and  $\Delta T_0$  at increasing fluence were observed for BAGIRA. A number of potential reasons have been excluded.



# EDF-4: basic information (1)

- ❑ EDF-4 is a 16MND5-type RPV steel taken from a shell ring of an RPV manufactured by Creusot-Loire
- ❑ Half-Charpy specimen of this material was provided by EDF
- ❑ CNRS contribution: comparison between chemical heterogeneities (microsegregations resulting from the solidification versus non-segregated areas)
- ❑ Methods: APT and TEM on samples in as-received and ion-irradiated conditions
- ❑ Composition:

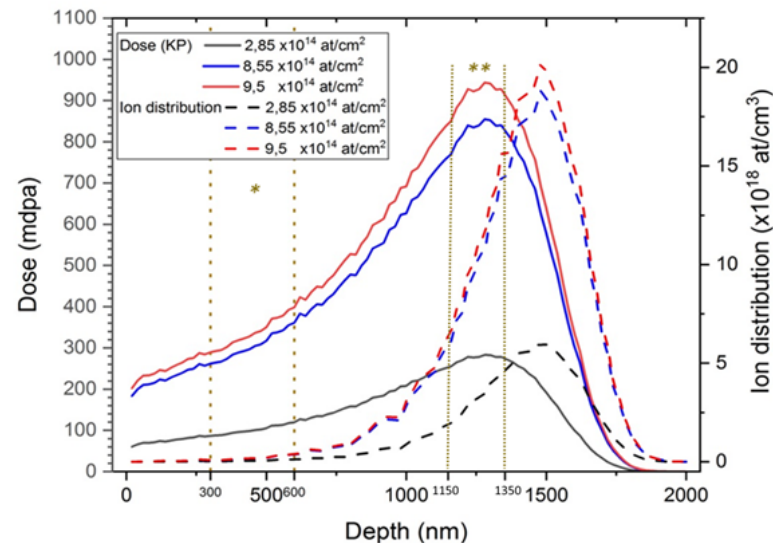
Material	Range	C	S	P	Si	Mn	Ni	Cr	Mo	V	Cu	Co	Al
EDF4	min	0.69	0.01	0.019	0.42	1.27	0.65	0.20	0.29	0.0087	0.61	0.019	0.045
	max												

# EDF-4: basic information (2)

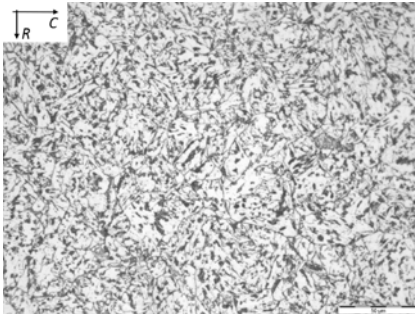
## □ Ion irradiation at Jannus

Nb.	Sample	Ion	Energy (MeV)	Fluence ( $10^{14} \text{ cm}^{-2}$ )	Flux ( $10^{10} \text{ cm}^{-2}\text{s}^{-1}$ )	Time (min)	Dose at APT analyses depth (dpa)	Dose rate ( $10^5 \text{ dpa.s}^{-1}$ )	T ( $^{\circ}\text{C}$ )
1	A239	$\text{Fe}^{3+}$	5	2.85	$1.6 \pm 0.4$	130	~0.1	1.3	400
2	* 4H3.3			8.55	5	296	0.26-0.34	1.7	
	** 4H3.3			9.5	4.4	360	0.78-0.85	4.5	
3	4H3.3			9.5	4.4	360	0.28-0.36	1.4	350

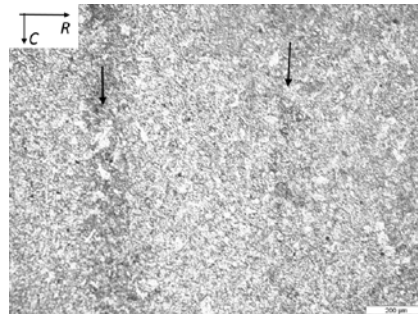
## □ SRIM calculations of the depth profiles of dpa and injected interstitials



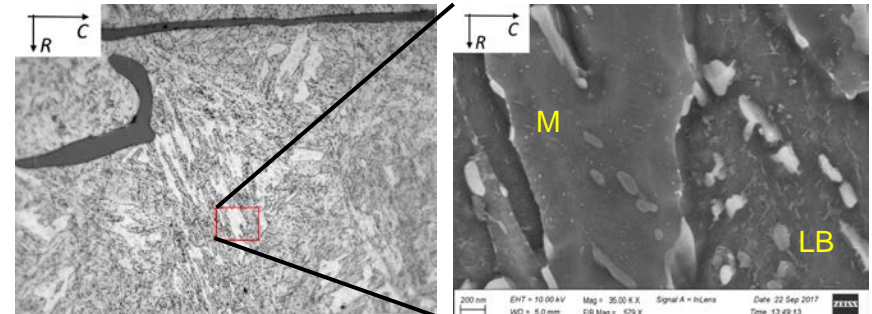
# EDF-4: initial microstructure



Segregation-free area  
Tempered upper  
bainite

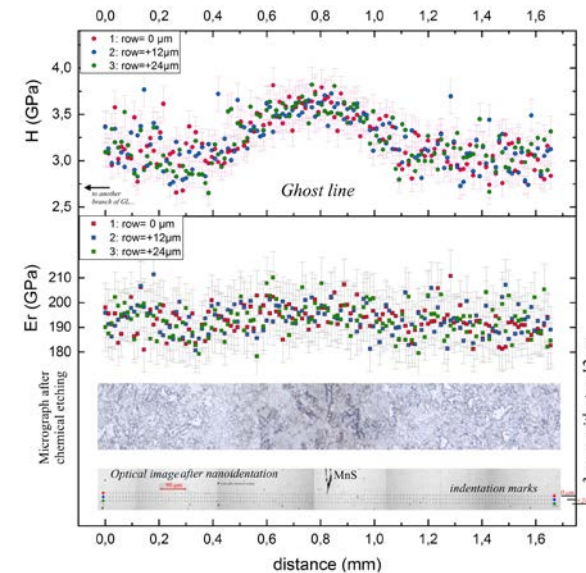
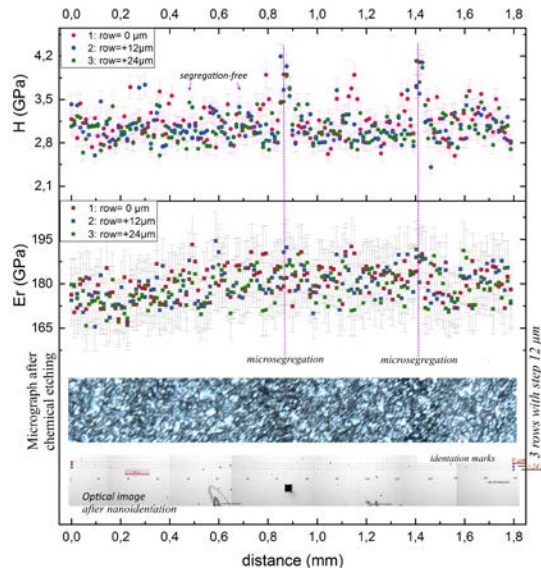


Microsegregations  
Tempered lower  
bainite



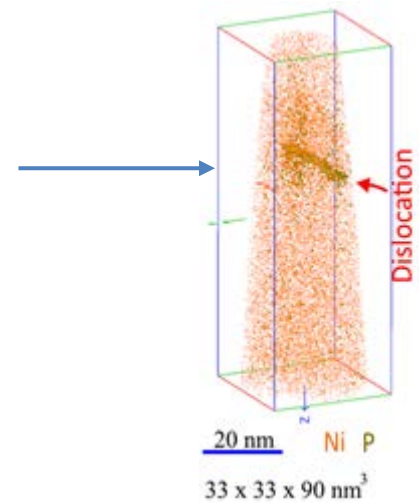
Macrosegregations (ghost lines)  
Tempered lower bainite (LB) and  
tempered martensite (M)

Nano-  
hardness



→ FIB lift-  
out of  
samples for  
APT  
and  
(S)TEM

- ❑ Occasional appearance of
  - NiSiMnP-enriched cluster in ion-irradiated sample from segregation-free area
  - MnNiSiMoCuP-enriched cluster in ion-irradiated sample from microsegregation area
- ❑ All ion-irradiated samples
  - P segregation to dislocations and GBs
  - Enrichment of dislocations with Mn, Ni and Si.
- ❑ No clear differences in the irradiation response between segregated and segregation-free areas were found.





# NRI-1 and -2: basic information

## NRI-1

- ❑ ASTM A 533B type IAEA reference steel known as JRQ,
- ❑ 160 t Ingot rolled into plates 225 x 2,500 x 3,000 mm,
- ❑ Final heat treatment: normalized at 900 °C, quenched from 880 °C, tempered at 665 °C for 12 hours.

	C	Mn	P	S	Si	Ni	Cr	Mo	Cu	V	Al
5JRQ	0.18	1.47	0.019	0.004	0.24	0.66	0.12	0.5	0.15	0.007	0.014

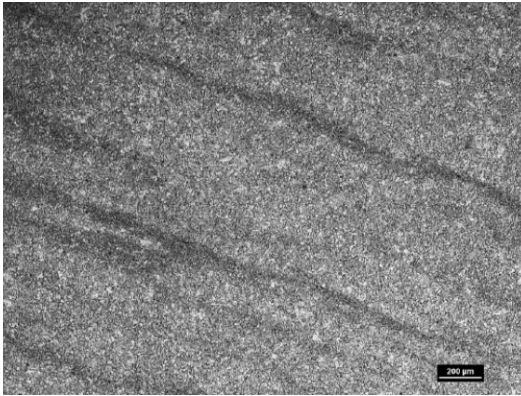
## NRI-2

- ❑ 15Kh2NMFAA type RPV steel for the beltline region of WWER-1000,
- ❑ Cylindrical ring, thickness 190 mm,
- ❑ Final heat treatment: normalized at 950-970 °C, quenched from 910-930 °C, tempered at 660-680 °C, annealed 640 °C.

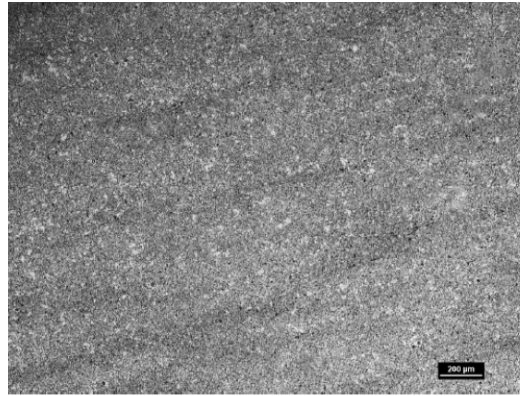
	C	Mc	Si	S	P	Cr	Ni	Mo	V
15Kh2NMFAA	0.15	0.46	0.22	0.012	0.008	1.54	1.34	0.53	0.12

# NRI-1 and -2: initial microstructure

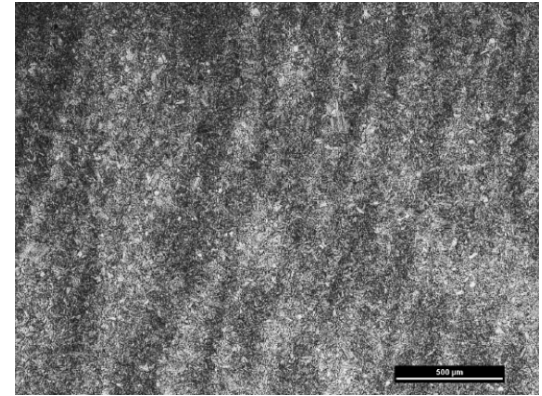
## □ NRI-1 (JRQ)



Layer 1 (5 mm depth)

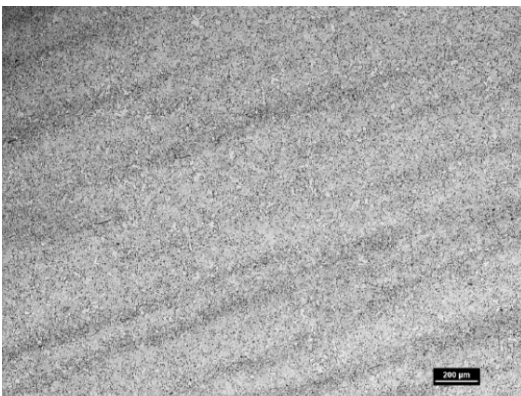


Layer 7 (113 mm depth)

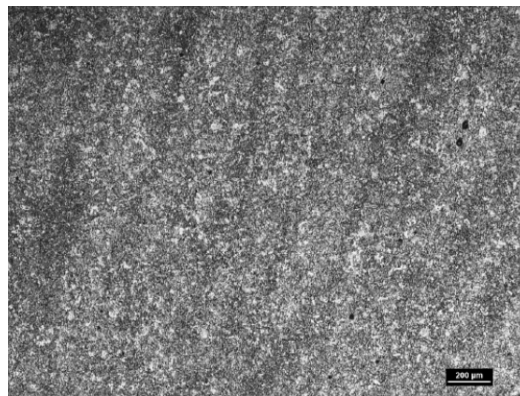


Layer 13 (220 mm depth)

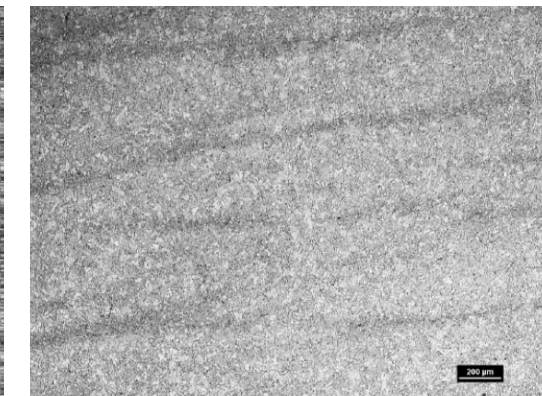
## □ NRI-2 (15Kh2NMFAA)



Layer 1 (5 mm depth)



Layer 6 (95 mm depth)

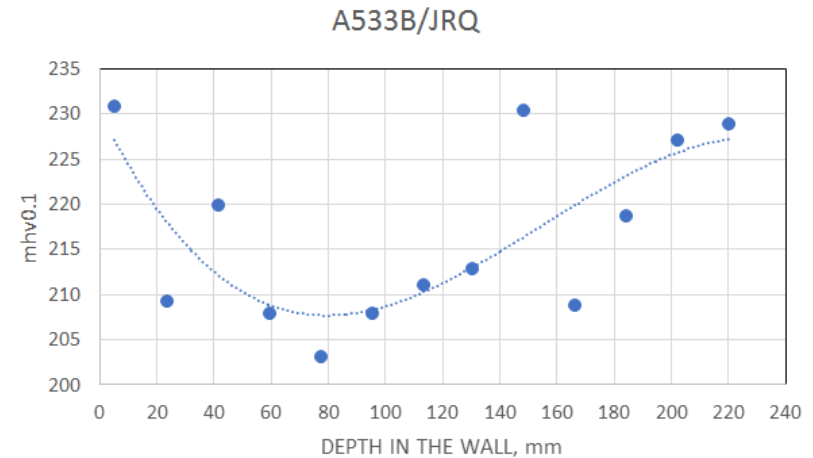


Layer 11 (185 mm depth)

# NRI-1 and -2: initial properties

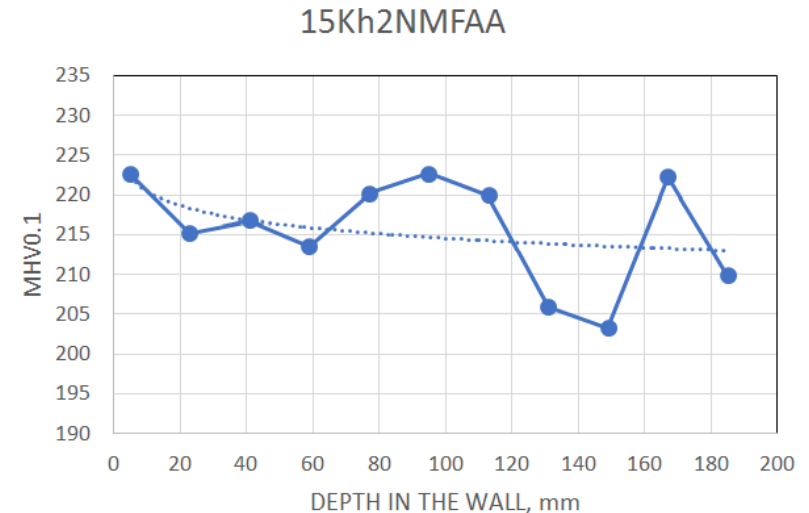
## □ JRQ

- characteristic through-thickness profile of HV0.1
- Segregation bands (270 HV0.1) harder than base (210 HV0.1)



## □ 15Kh2NMFAA

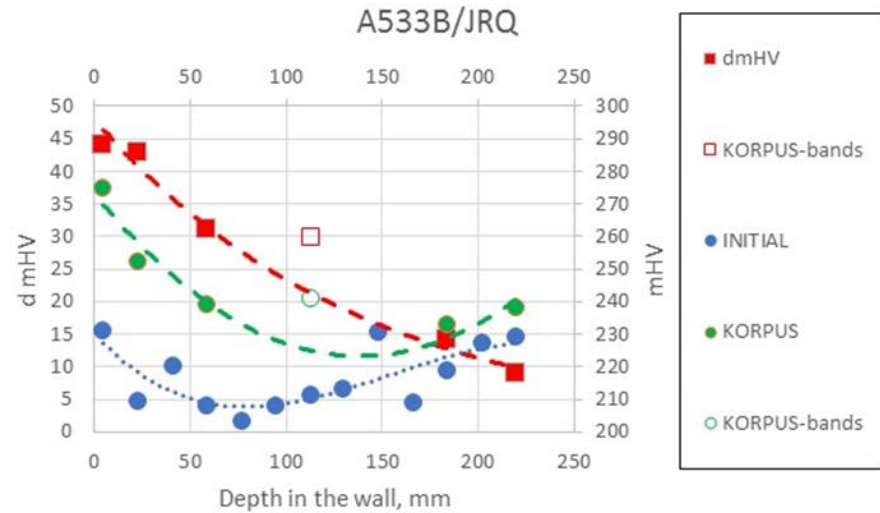
- HV0.1 approximately const.



# NRI-1 and -2: irradiation hardening

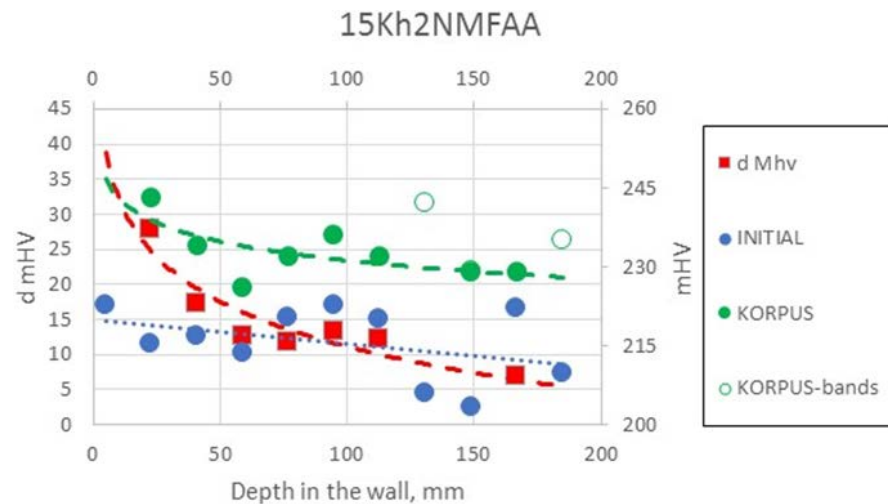
## □ JRQ

- Irradiation-induced increase of HV0.1
- $\Delta HV0.1$  almost equal for segregation bands and segregation-free area



## □ 15Kh2NMFAA

- Irradiation-induced increase of HV0.1





- ❑ Segregation bands clearly identified
- ❑ Irradiation-induced nanofeatures and hardness increase observed
- ❑ Segregation-free areas, microsegregations and macrosegregations
  - exhibit different microstructures and hardness
  - do not exhibit differences in the irradiation response
- ❑ Differences in the fracture behaviour (irr. versus unirr.) have not been addressed but are expected

# ANP/VTT: basic information (1)



- ❑ Four irradiated materials were investigated:
  - PWR 22NiMoCr3-7 base materials ANP-3 and ANP-4 (Klöckner)
  - VVER-440 10KhMFT weld materials VTT-1 and VTT-MW1

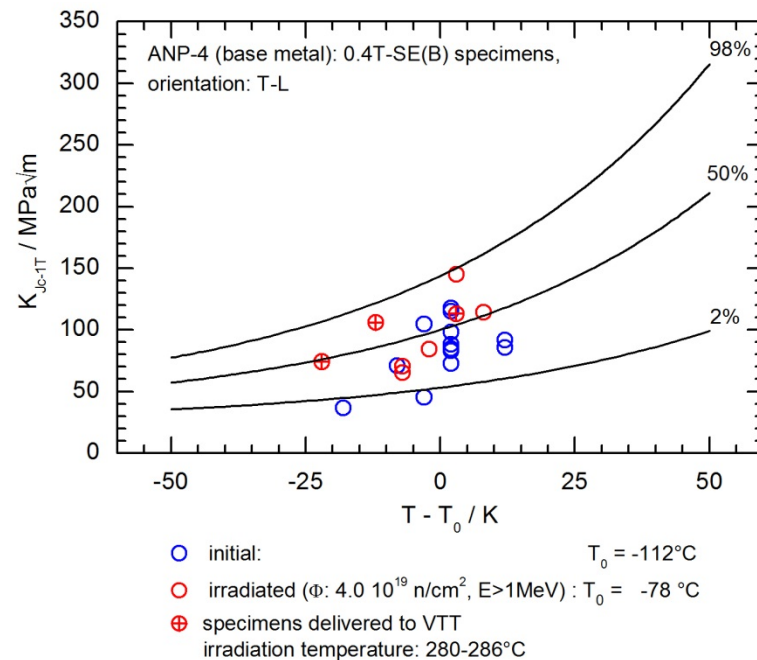
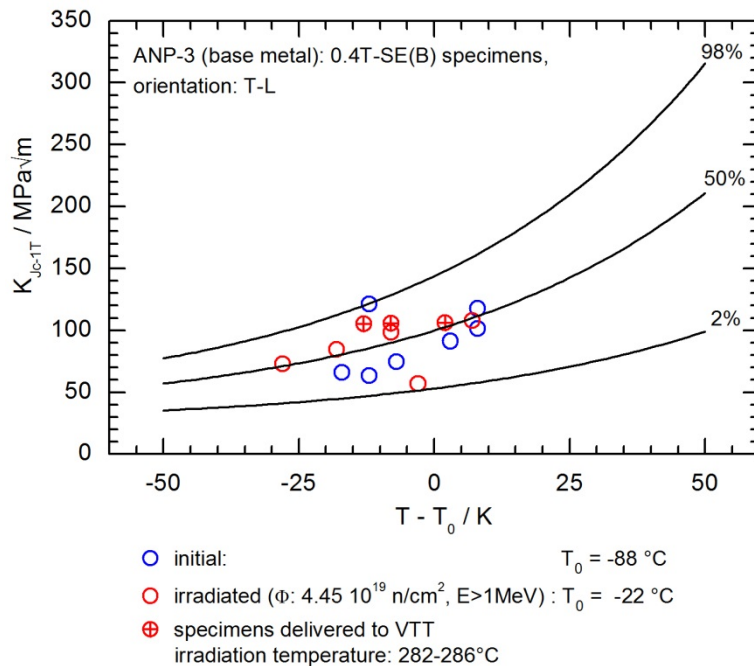
	C	Si	Mn	P	S	Cr	Mo	Ni	Al	Co	Cu
ANP-3	0.23	0.20	0.70	0.015	n.s.	0.44	0.79	0.98	n.s.	n.s.	0.12
ANP-4	0.182	0.234	0.926	0.005	0.005	0.408	0.478	0.886	0.020	0.012	0.062
VTT-1	0.04	0.6	1.06	0.02	0.026	1.57	0.46	0.13	n.s.	n.s.	0.19
VTT-MW1	0.05	0.4	1.2	0.038	0.011	1.4	0.49	0.14	n.s.	n.s.	0.17

- ❑ Fractographic examination focused on
  - finding the primary cleavage initiation site
  - identifying any microstructural features or heterogeneities that may have promoted fracture in the irradiated condition.



# ANP/VTT: basic information (2)

## □ ANP samples investigated: ⊕

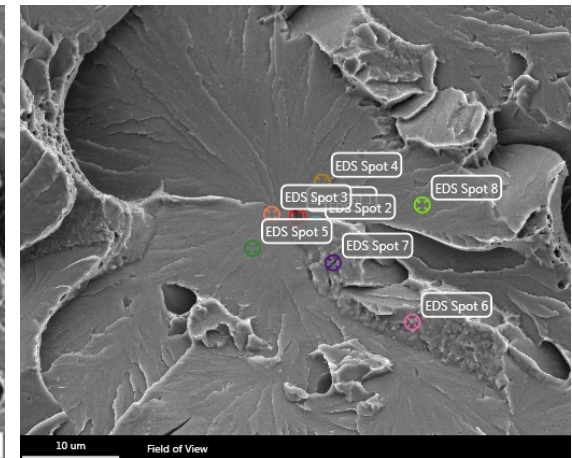
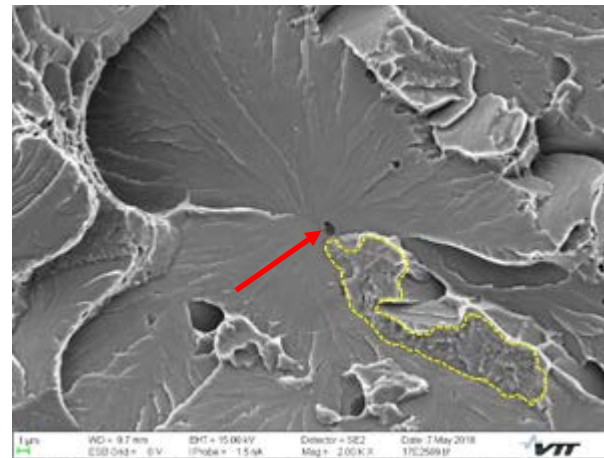
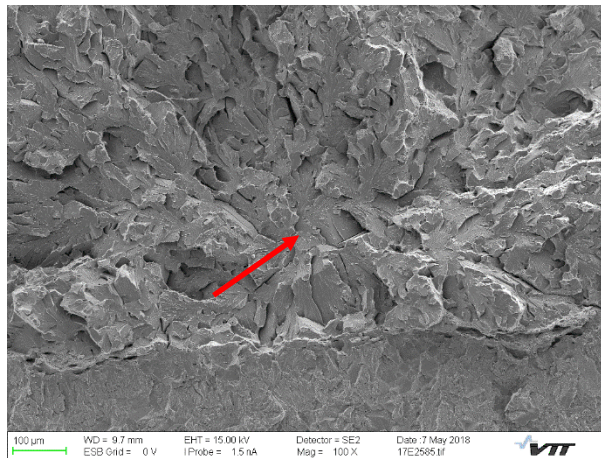
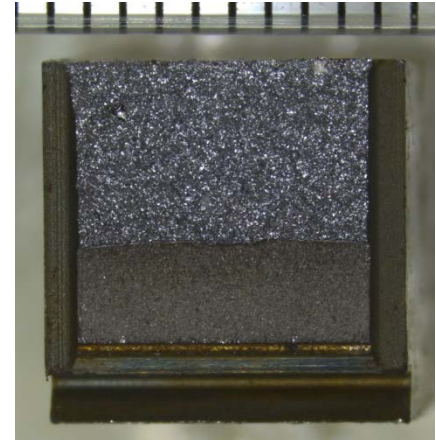


## □ Optical, fractography, SEM-EDS performed at VTT

# ANP/VTT: initiation sites (1)

## □ ANP-3

- left: overview (cleavage initiation site marked)
- middle: cleavage initiating particle (marked)
- right: spots for SEM-EDS analysis





# ANP/VTT: initiation sites (2)

Material	Specimen	Cleavage initiation site	Type of initiating particle
ANP-3	BA28	Primary Initiation site Not visible, as it locates under a ledge	No visible particle
ANP-3	BA32	Primary initiation site particle	Cr-, Mn-, Mo- (+ S), Co- and O-rich particle Cr, Mn, Co = half A Mo (+ S), O = half B
ANP-3	BA35	Primary initiation site particle	Probably a Mn-, Cr-, Mo- (+ S), Al-, O-rich particle half A only no particle on half B
ANP-4	2BTL3	Primary initiation site	No clear particle
ANP-4	2BTL9	Primary initiation site particle	Probably a Mn-, Mo- (+ S), S-, Cr-, C- and O- rich particle Mo (+ S), Cr, Mn, O = half A Mo, S, Cr, Mn, O = half B
ANP-4	2BTL14	Primary initiation site	No particle visible
VTT-1	L22_17I209	Initiation site	No particle visible
VTT-1	L22_18I204	Initiation site Particle	Al-, Si-, S-, Ti-, Mn- and O-rich particle
VTT-1	L24_17I204	Initiation site Particle	Al-, Si-, Ti-, Mn- and O-rich particle
VTT-MW1	132M	Initiation site Particle	Al-, Si-, Ti-, V-, Mn- and O-rich particle
VTT-MW1	172	Initiation site Particle	Al-, Si-, Ti-, Mn- and O-rich particle
VTT-MW1	311	Initiation site Particle	Si- and O-rich particle

- ❑ Initiation sites identified and distance from the sample side face statistically evaluated
- ❑ ANP-3 and ANP-4
  - in three out of 6 cases visible particles enriched with Cr, Mn, Mo (S), Al, O
  - initiating particles might be MnS or Cr-, Mn-, Al-oxides or combinations of both
- ❑ VTT-1 and VTT-MW1
  - initiating particles typically Al-, Si-, Ti-, Mn-, O-rich
- ❑ Initiation at carbides was not reported

# Task 3.3: lessons learned



- ❑ Six partners – eight materials – four approaches – many pieces of new insight
- ❑ Initial inhomogeneity may be
  - alleviated by irradiation (scatter of MC decreased)
  - retained after irradiation (segregated and segregation-free areas exhibit similar irradiation response, IGF)
  - intensified by irradiation (no example found → good message)
- ❑ Remaining gaps (personal view)
  - systematically correlate outliers in MC curves with local microstructure (segregated or segregation free-areas)
  - systematically compare initial distribution of coarse particles with type of particles initiating cleavage

