

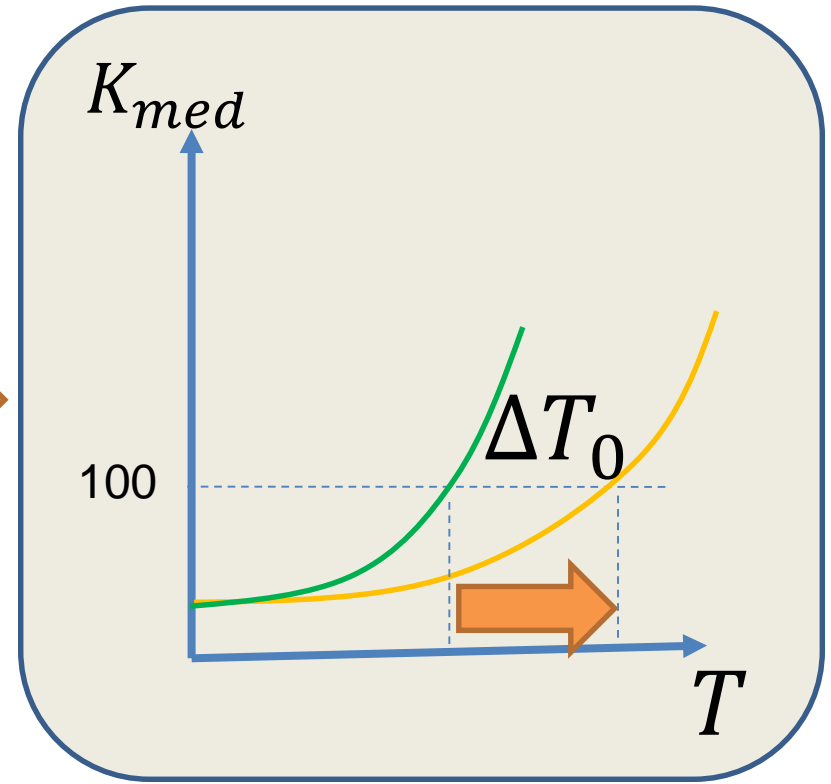
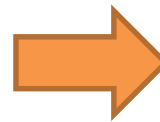
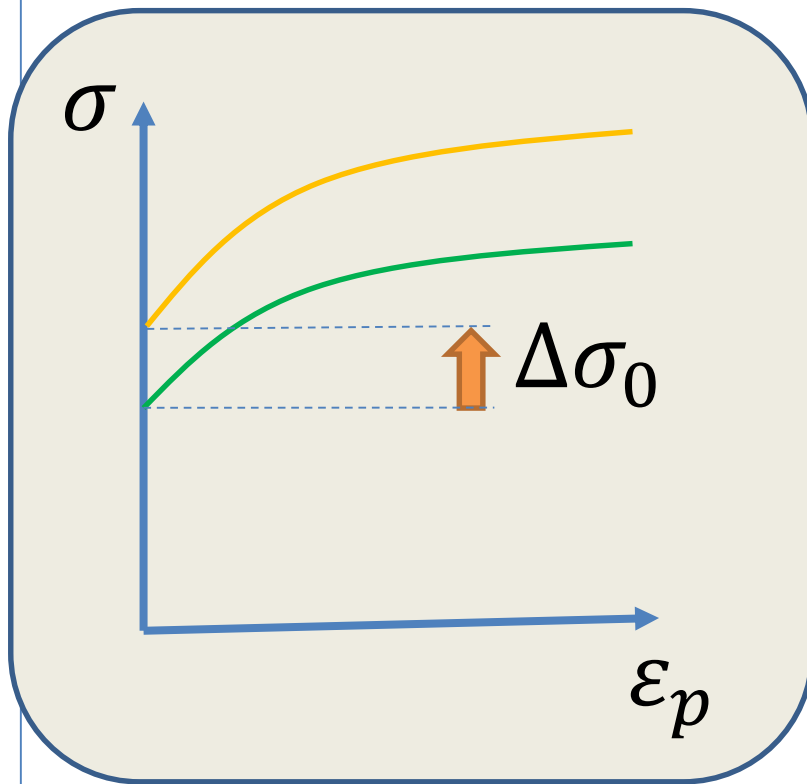
INTERACTIVE SESSION III : RPV EMBRITTLEMENT COMPUTING A DUCTILE-BRITTLE TRANSITION TEMPERATURE T_0 USING A LOCAL APPROACH TO FRACTURE

A. Marchenko

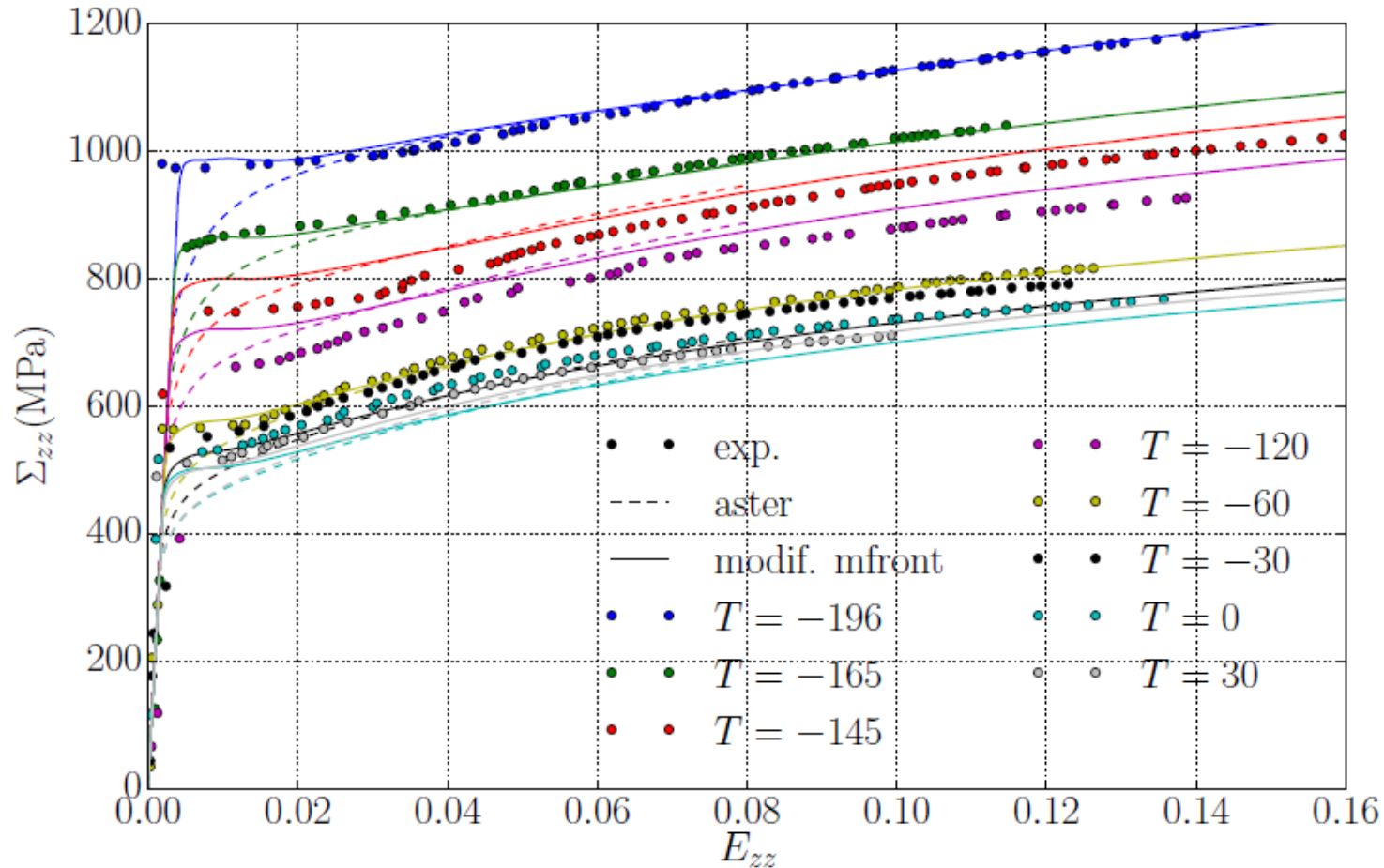
P. James



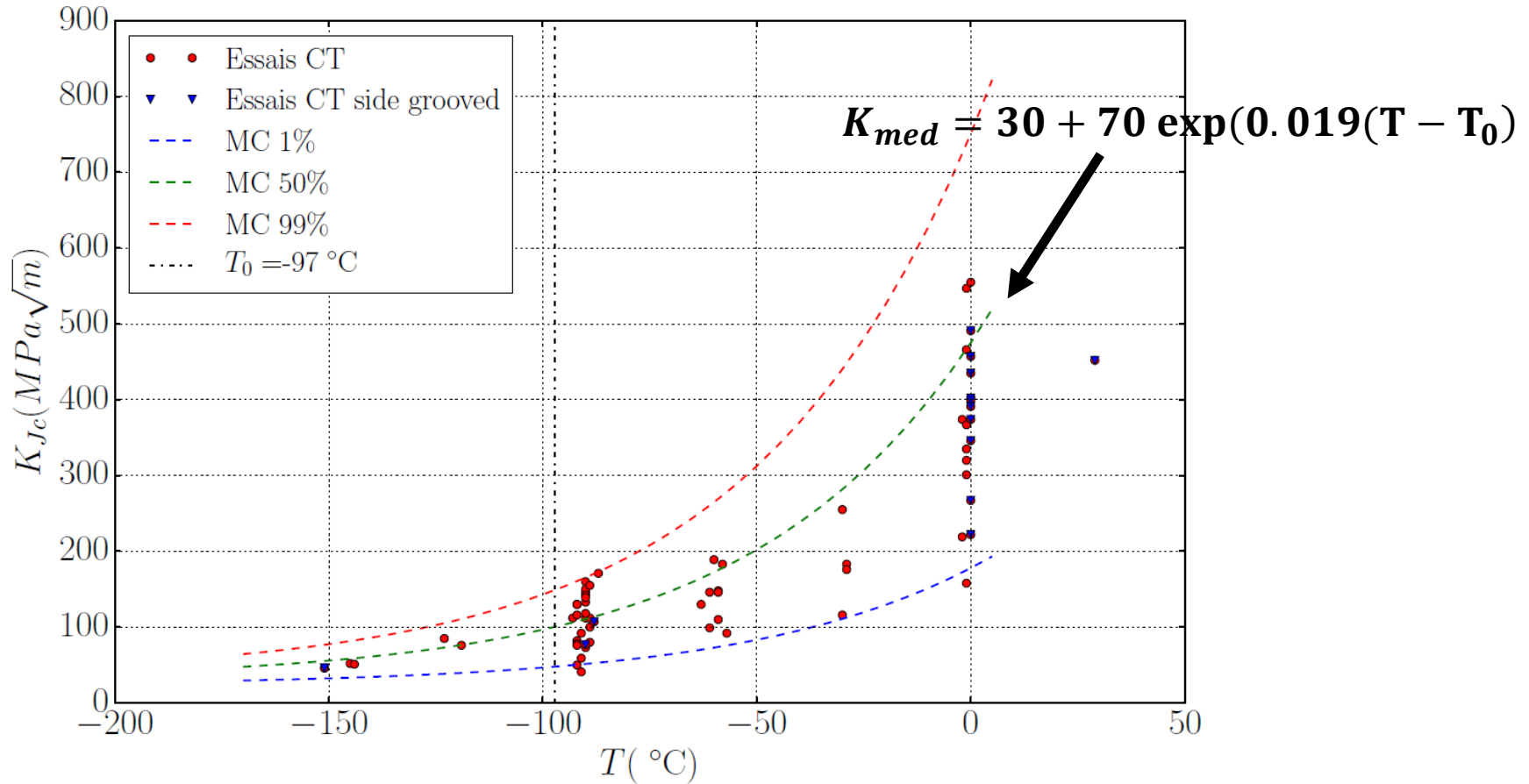
Exercise Objective



H1BQ12 Steel tensile properties



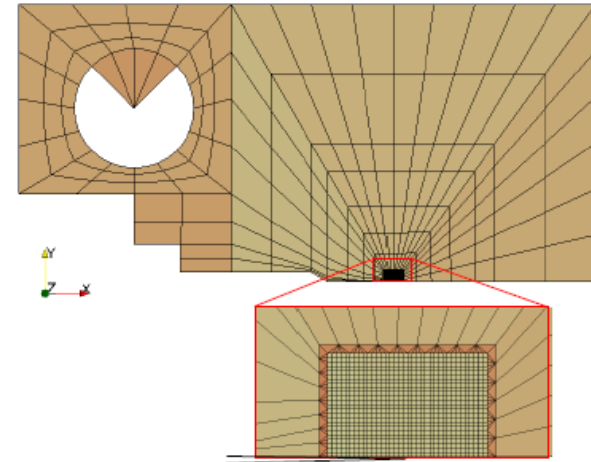
H1BQ12 Steel fracture properties



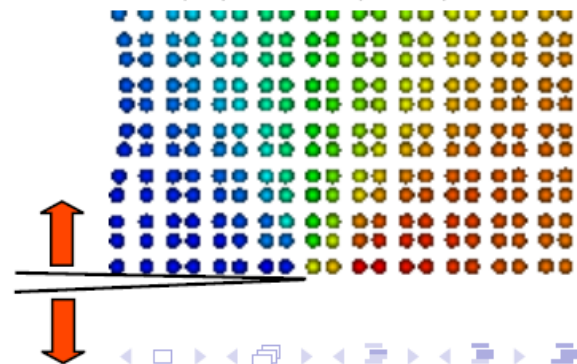
Master Curve

$$P_f(K_{Jc} \leq K) = 1 - \exp \left[- \frac{B}{B_0} \left(\frac{K - K_{min}}{K_{med} - K_{min}} \right)^4 \right]$$

- To circumvent the limitations of the Master Curve approach, the local approach to failure proposes a **chaining** of a **plastic** calculation and a **failure** post-treatment
- The plastic calculation proposed in the platform is available in the RPV Toughness Module as "CTCalculation"
- It is a 2D calculation using Code_Aster as solver
- possible chainings with homogenized **crystal plasticity law** to benefit from lower scale plastic models



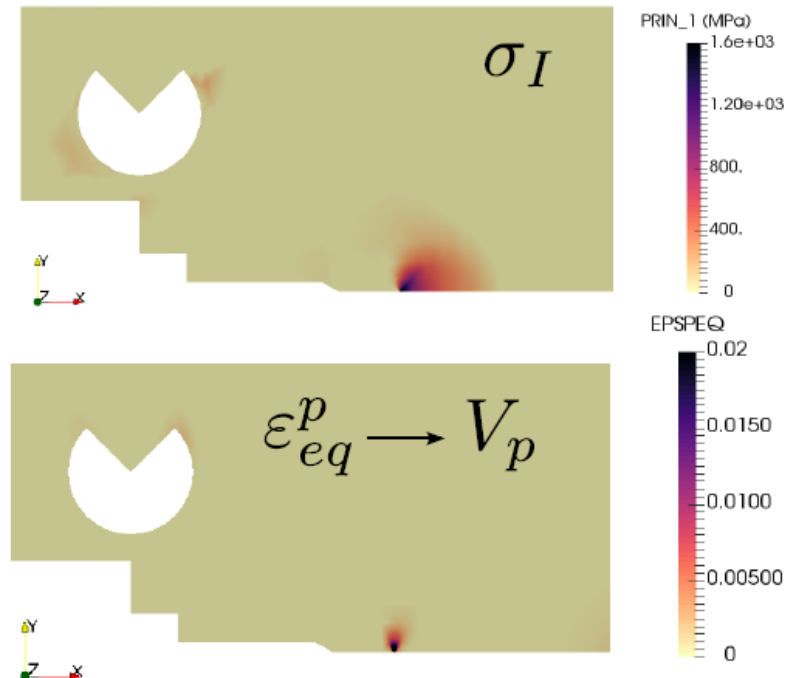
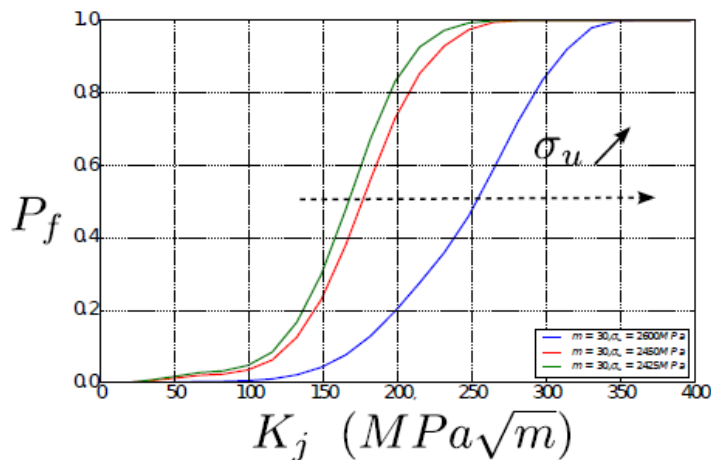
$$\sigma_I(x) = f(K_J)$$



- $\forall K_j(t_i)$
- fitting a Weibull stress σ_W on the plastic Volume V_p using the σ_I field
- Compute the failure probability P_f

$$\sigma_W = \left(\int_{V_p} \sigma_I^m \frac{dV}{V_0} \right)^{m^{-1}}$$

$$P_f = 1 - \exp \left[- \left(\frac{\sigma_W}{\sigma_u} \right)^m \right]$$

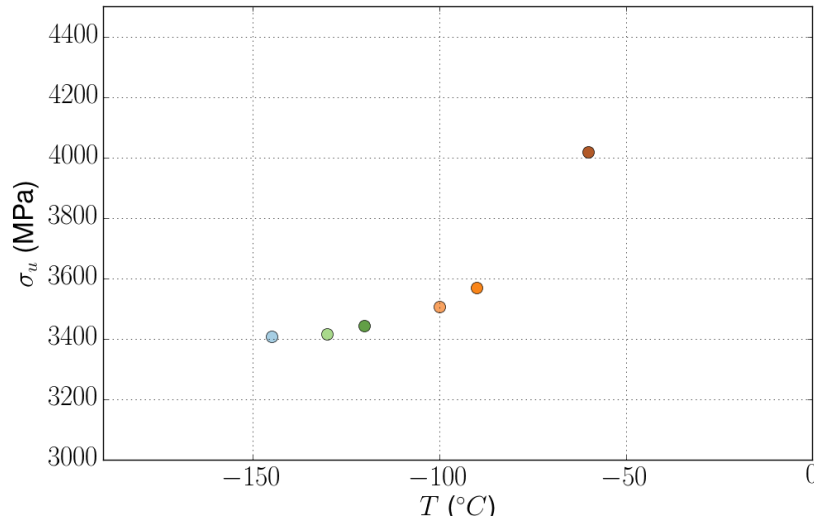
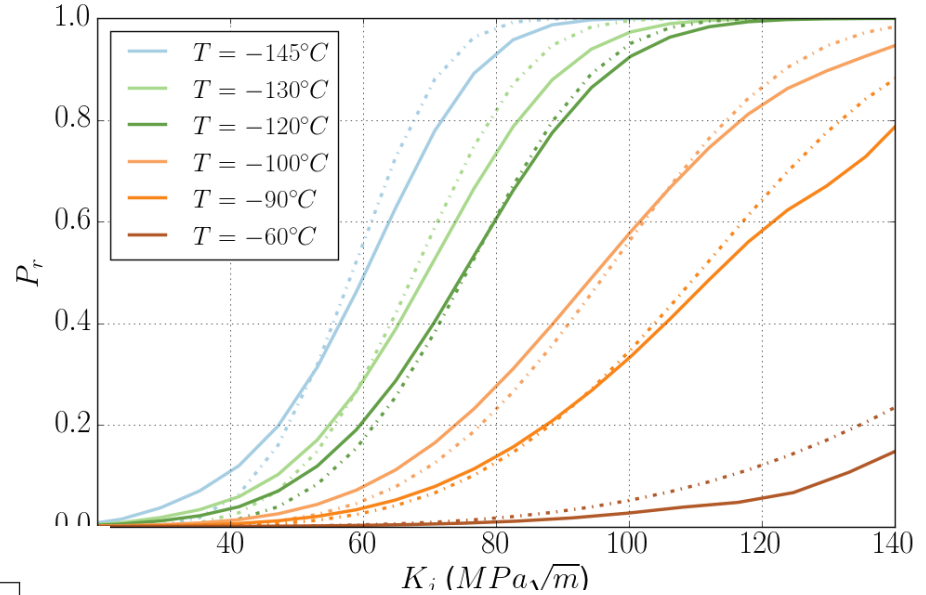


- Beremin parameters : m, σ_u, V_0

Correlation Beremin – Master Curve



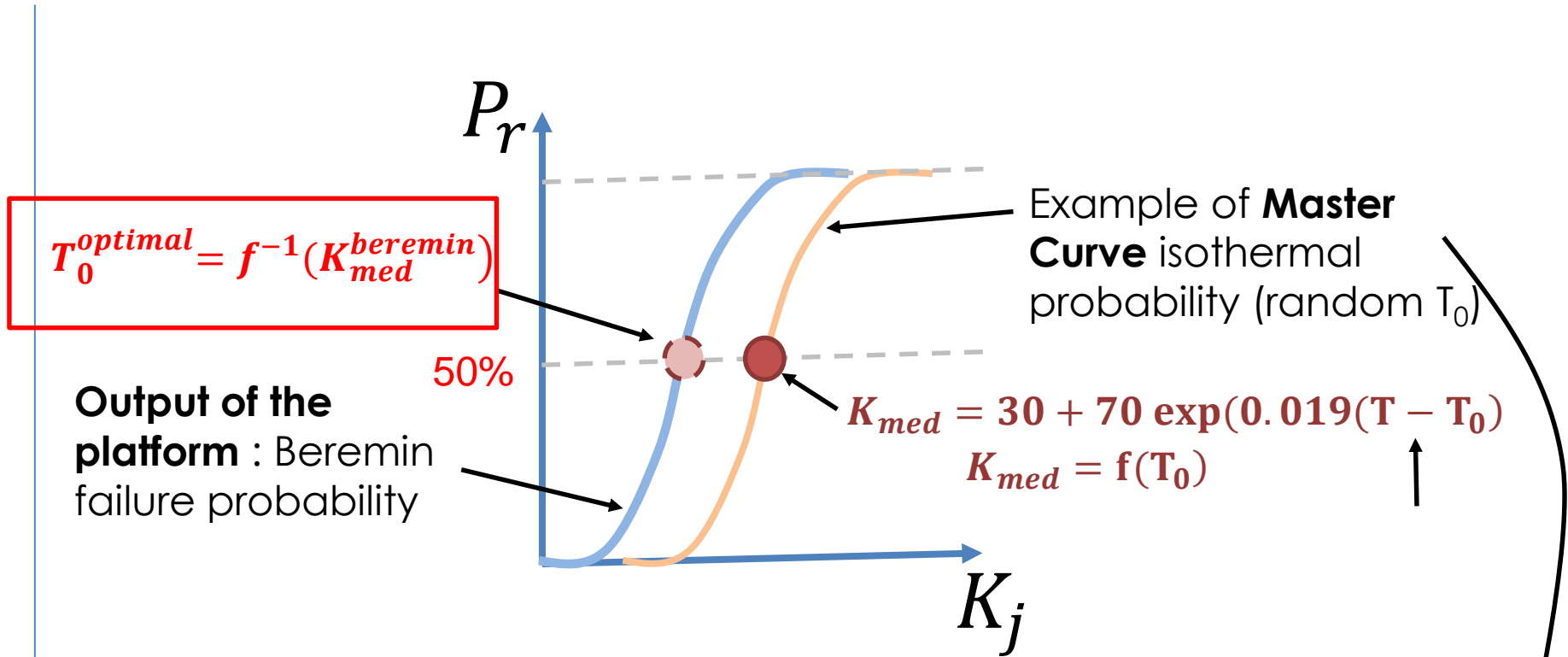
Solid Line = Beremin
Dashed Line = Master Curve



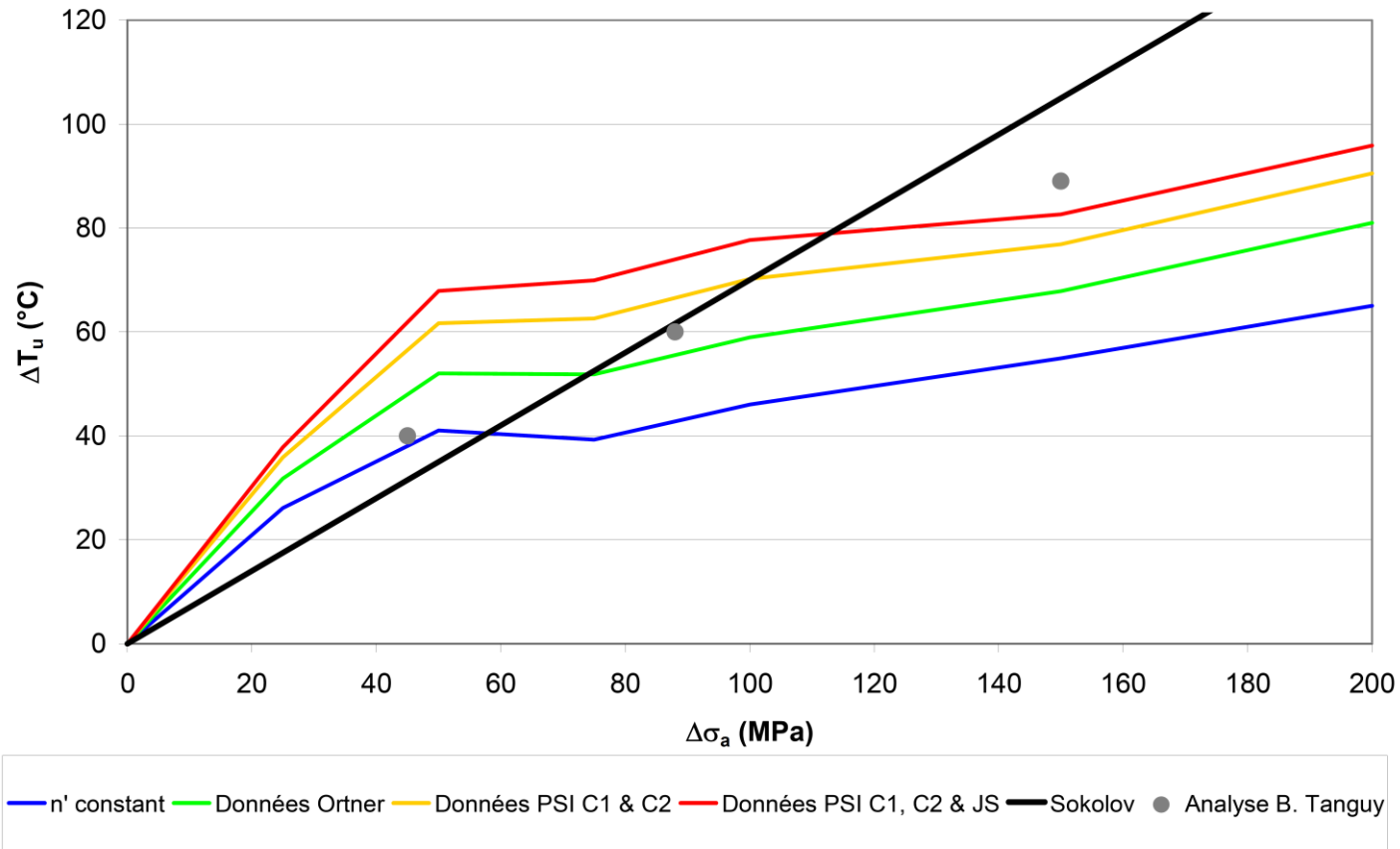
$$\sigma_u = A + B \exp(C T)$$

A (MPa)	B (MPa)	C
3267	961	0.025

Fitting T_0 with MasterCurve



$$P_f(K_{Jc} \leq K) = 1 - \exp \left[-\frac{B}{B_0} \left(\frac{K - K_{min}}{K_{med} - K_{min}} \right)^4 \right]$$



$$\sigma_u = A + B \exp(C (T - \Delta T_u)),$$

$$\Delta T_u = \Delta T_0,$$

$$\Delta T_0 = \alpha \Delta \sigma_0, \quad \text{with } \alpha = 0.7$$

B.Tanguy, A. Parrot

Sokolov relation

Modules chaining

list of available modules

chain

